#### Robotics research in Odense

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## **SDU Robotics**





#### Education

#### **Robot systems Engineering**

M.Sc. (2 years) (Intake 2019: 60 students),

BSc (MSc) (3 (5) years) (Intake 2019: 60 students) Cutoff: 8.0

B.Eng.

(Intake 2018: 90 students)
Total: Around 210 new students

#### **Welfare Technology**

M.Sc., B.Sc.

(Intake: around 30 students)





#### Research

#### **Robot Control**

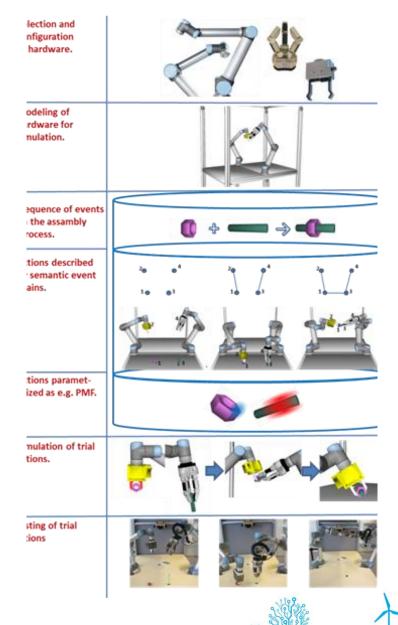
- Kinodynamic modelling and planning
- Force-based control
- Process Optimization

#### **Computer Vision**

- Object recognition and Pose estimation
- Optical issues in Computer Vision
- Inspection (NEW)

#### **Model Based Robot Systems Engineering**

- Digital Twins
- Visual Programming
- Co-simulation with MATLAB, ROS, ...







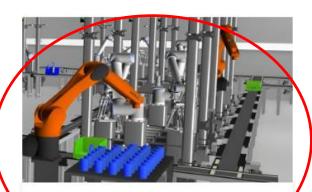
Robotic Solutions for Industrial



Welfare Robotics



Surgical Robotics



Mathematical Modelling and Simulation of Robotic Systems and Processes



Computer Vision based Object Recognition and Pose Estimation

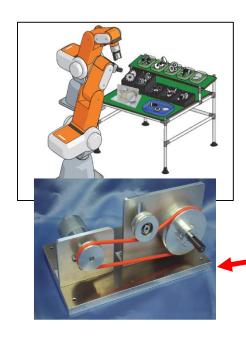


Model and Learning-based Control of Robotic Systems

## Industrial Robotics World Robotic Challenge

#### SDU Robotics wins the "unofficial World Cup" in industrial robotics

- 4 day competition in Tokyo in October 2018
- 16 teams selected from 250 applicants
- Relevant industrial assembly challenges









## History

- Unimate 1956-70
  - Hydraulic



- 1970's
  - Electric
  - Up to 6 degrees of motio⊢



#### Pictures of different robots









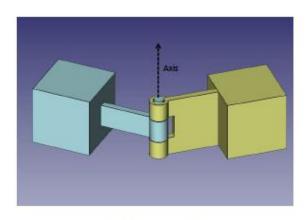




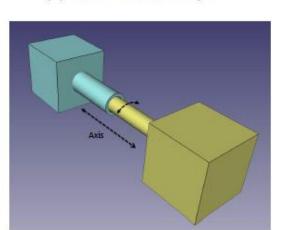
The next 23 slides will illustrate why an industrial robot manipulator arm is just a stupid machine that is easy to use as any other tool...



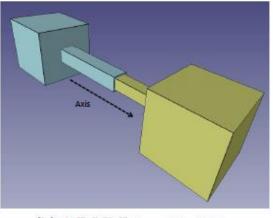
## Robot joints



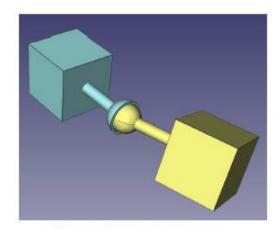
(a) 1 DOF Revolute joint.



(c) 2 DOF Cylindrical joint



(b) 1 DOF Prismatic joint.



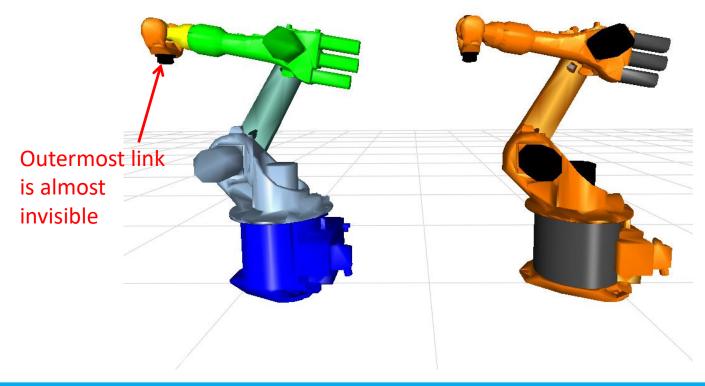
(d) 3 DOF Spherical joint



Figure 2.1: Joint types.

#### **Robot links**

Links marked with different colours





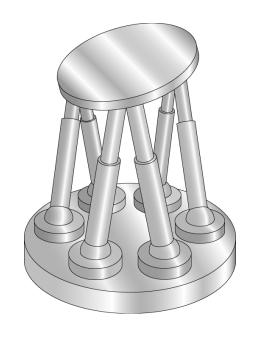
#### Constraints on Actuation and Topology

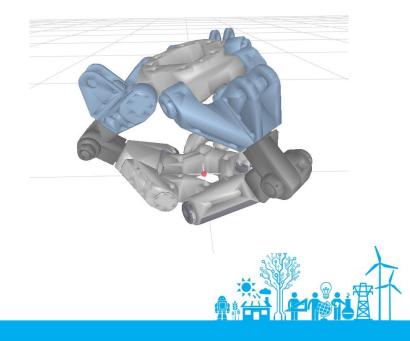
- The robot consists of a set of links and joints connected into a single structure
- Any two links are connected by at most one joint.
- Some, but not necessarily all, joints are motorized
- Each motorized joint can move independent of the other motorized joints.
- If all motorized joints are fixed at a given position, the robot will be kinematically stiff (typical case). Otherwise the robot is underactuated.



## Robots with Closed Loop Topology

 The robot consists of a set of links and joints connected into a single structure





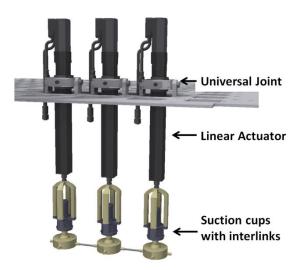
## Palletizing robot with 4-bar linkages



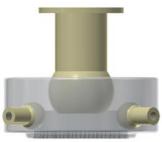


#### **Underactuated Robot**





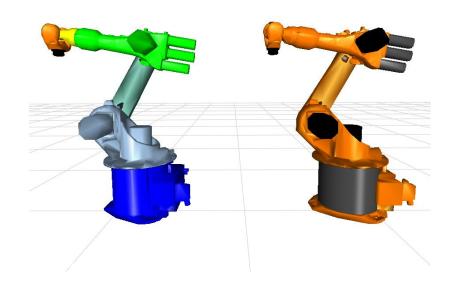






#### Kuka KR16

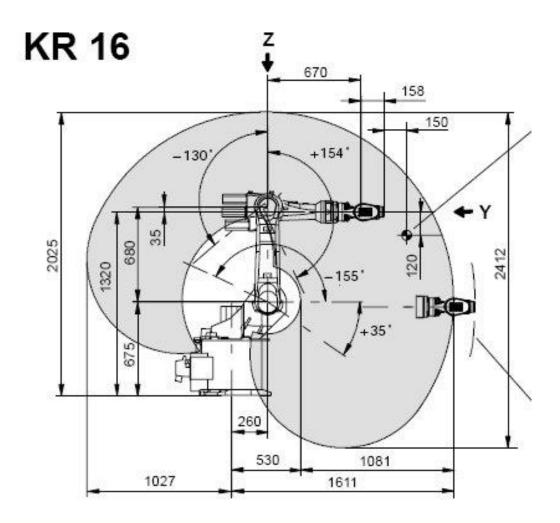
How do we describe the kinematics?





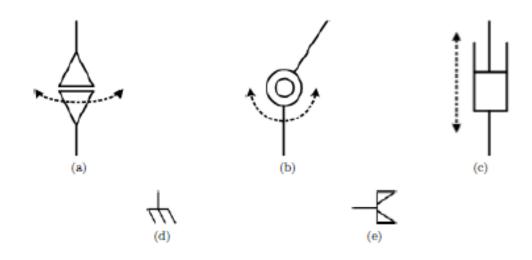
#### Kuka Kr16

#### Typical drawings



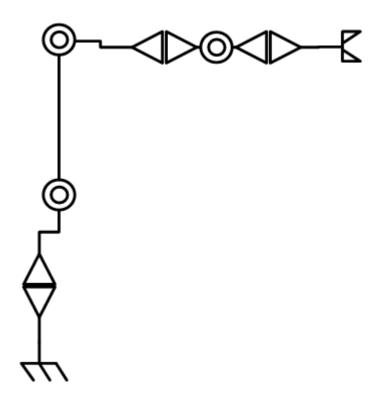


### Joints, base and tool



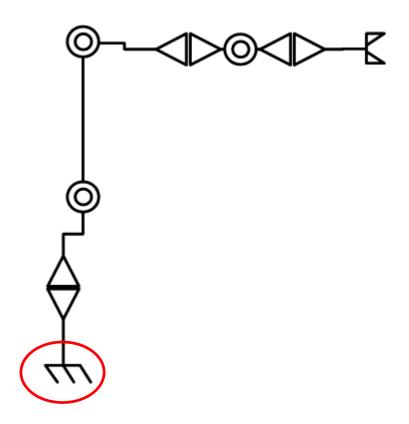
- a): Revolute joint (vertical rotation axis)
- b): Revolute joint (rotation axis perpendicular to drawing plane)
- c): Prismatic (translational) joint
- d) Robot base
- e) Robot tool





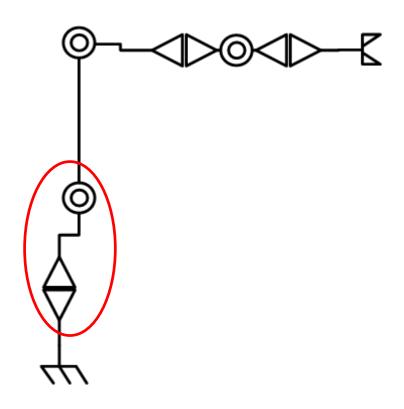


(Robot) Base



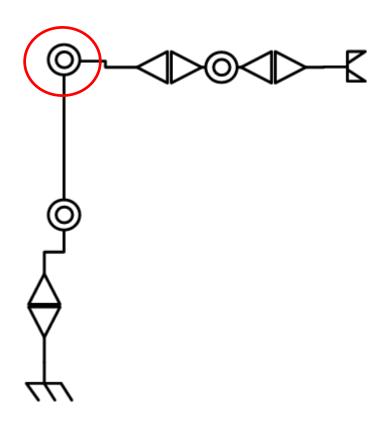


Shoulder joints (2)



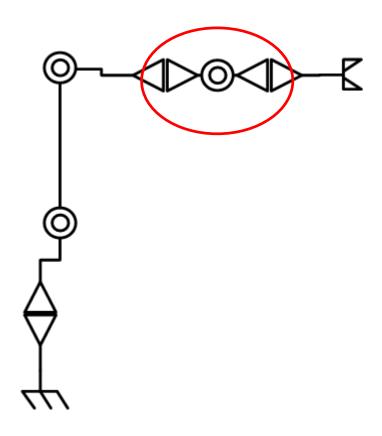


Elbow joint (1)

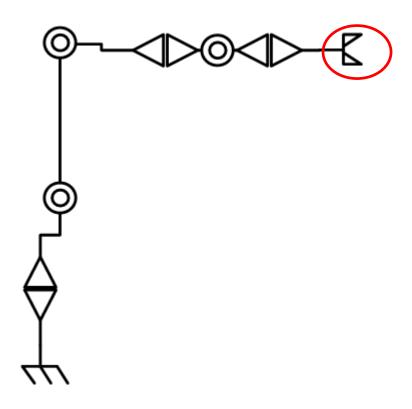




Spherical wrist (3)

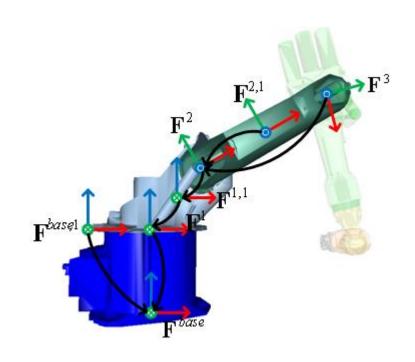






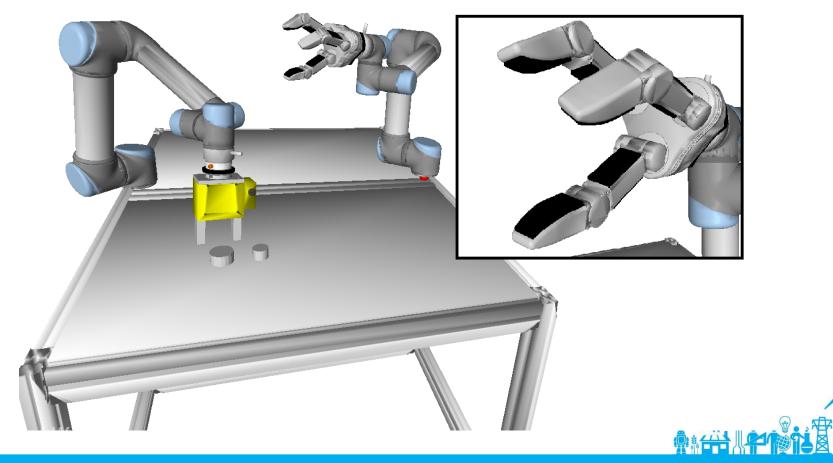


#### Frames on a robot

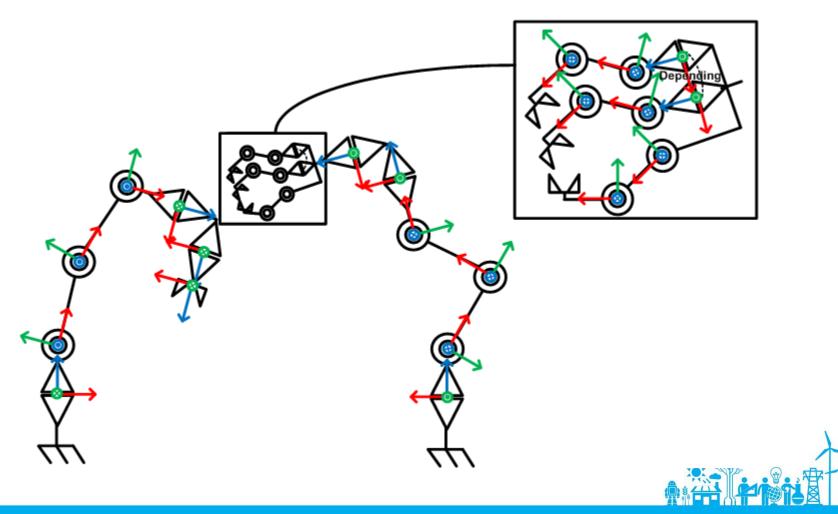




#### A two robot work cell

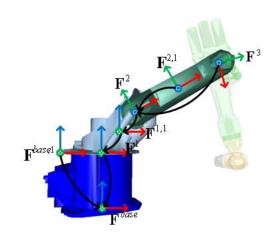


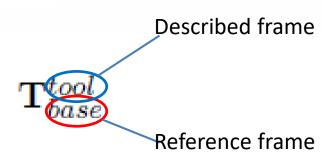
#### Frames in a work cell



## Homogeneous Transformation

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0}_{1 \times 3} & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & x \\ r_{21} & r_{22} & r_{23} & y \\ r_{31} & r_{32} & r_{33} & z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$







#### Joint vector q

• The *joint vector* is defined as the set of all joint variables of all robotic devices in a scene

 To simplify, we will from now on only consider a single serial robot in a scene.

 The joint vector uniquely determines the position and orientation of all robot links

#### Tool frame and Forward Kinematics

The *tool frame* is a special frame fixed with respect to the outermost link on the robot.

It defines the position and orientation of the active site on the robot (for simplicity we assume that there is only one active site).

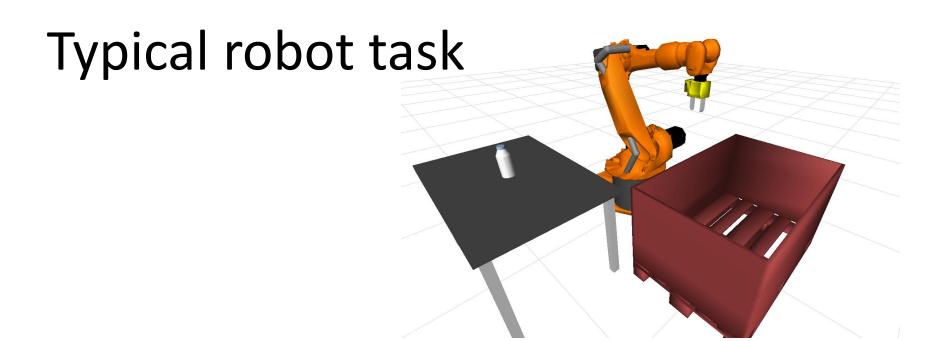
We denote it by the homogeneous transformation :  $\mathbf{T}_{base}^{tool}$ 

Forward kinematics is the task of computing the tool frame as function of the joint vector, denoted as  $\mathbf{T}_{base}^{tool}(\mathbf{q})$ 

The task is accomplished by straightforward use of matrix algebra

$$\mathbf{T}_{base}^{tool} = \mathbf{T}_{base}^1 \mathbf{T}_1^2 \dots \mathbf{T}_{n-1}^n \mathbf{T}_n^{tool}$$





**Move**  $\mathbf{F}^{1a}$  //Collision free move to frame  $\mathbf{F}^{1a}$  where the tool is adjacent to the bottle

Move Linear to frame  $F^{1b}$  //Move the tool in a straight line to the bottle

Close Gripper //Pick up the bottle

**Move Linear to frame F^{1a}** //Move back to frame  $F^{1a}$ 

**Move F^{2a}** // Colllision free move to frame  $F^{2a}$  adjacent to the place position at the table

**Move Linear to frame F^{2b}** //Move the tool in a straight line to the place position

Open Gripper //Release the bottle

Move Linear to frame  $F^{2a}$  //Move back to frame  $F^{2a}$ 

**Move Home** //Move back to the *Home* configuration



#### **Inverse Kinematics**

Desired transformation  $[\mathbf{T}_{base}^{tool}]_{desired}$ 

Find a joint vector  $\mathbf{q}$  so that  $\mathbf{T}_{base}^{tool}(\mathbf{q}) = [\mathbf{T}_{base}^{tool}]_{desired}$ 

Nonlinear root finding problem.

Numerical approach – for any serial robot. Good initial guess required

Find all joint vectors  $\mathbf{q}$  so that  $\mathbf{T}_{base}^{tool}(\mathbf{q}) = [\mathbf{T}_{base}^{tool}]_{desired}$ 

Analytical approach – for serial robots with special (idealized) kinematics.



The previous 23 slides has illustrated why an industrial robot manipulator arm is just a stupid machine that is easy to use as any other tool...

## Challenges in industrial robotics are related to describing and optimizing the process

- Modelling the process
- Use the model to derive a desired robot tool path
- Complete the solution by inverse kinematics



#### Why work with industrial robotics?

#### Human workers

- Movable so that they can go to where the work in the shopfloor is
- Fast start-up (hours for new tasks, immediately for shifts between existing tasks)
- Humans quickly learn how to improve the performance based on experience
- Easy adaptable to task modifications

#### Traditional automated solutions

- Static big facilities with fences and a lot of integrated machinery
- Slow start-up (typically in the range of 3-24 months for new tasks)
- Improvement based on experience is basically non-existing
- Difficult to adapt to task modifications
- (Much) too expensive, i.e. too long payback time except for "long term high runners"



# Traditional robot automation Complex, but repetitive

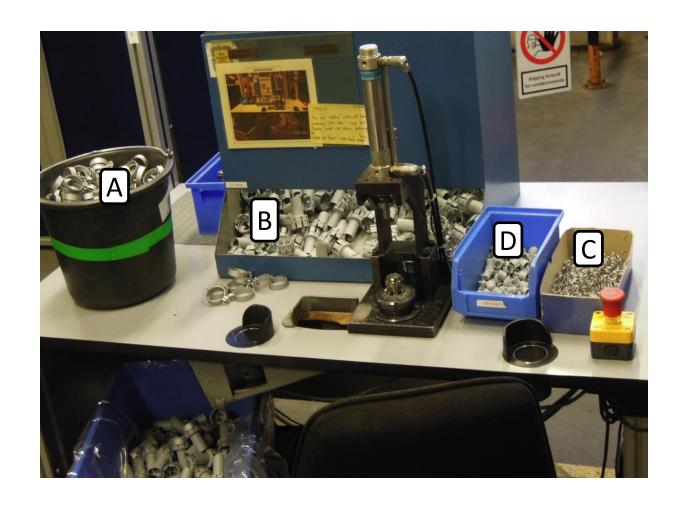




# Traditional robot automation Non-repetitive, but simple

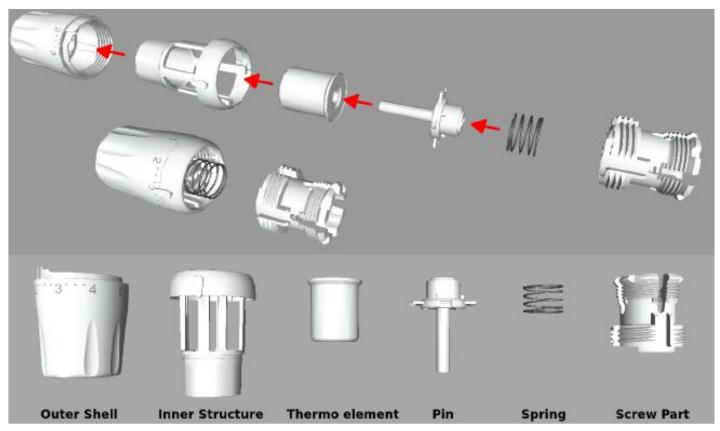


# Trend in robotic automation Non-repetitive and (somewhat) complex





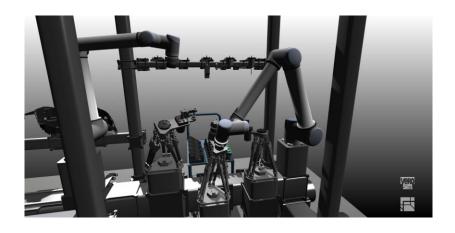
# Trend in robotic automation Robot programming based on digital models





#### Programming and testing in virtual environments

Example from one of our European projects: Headlight assembly for automotive

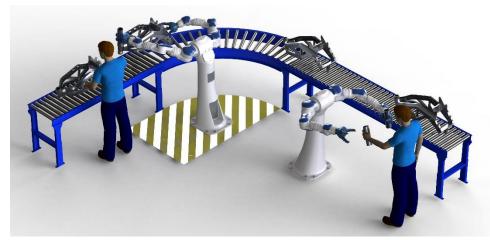






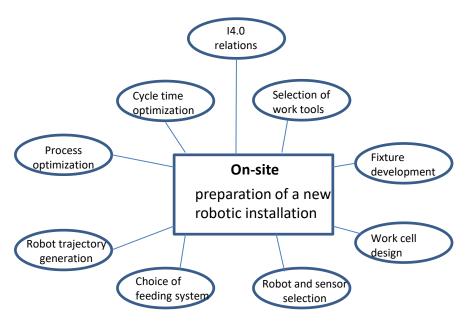
# Trend in robotic automation Collaborative robots







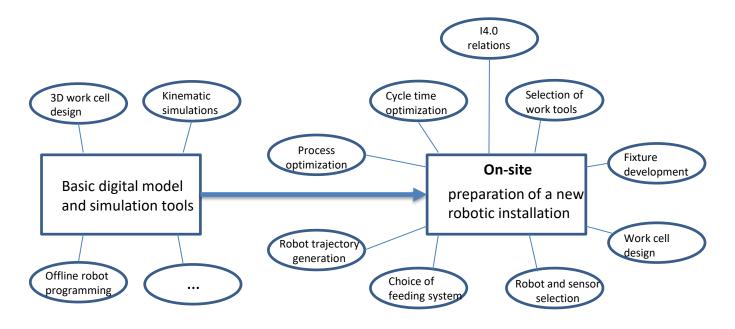
#### Traditional programming of robot systems







#### Using just simple digital tools



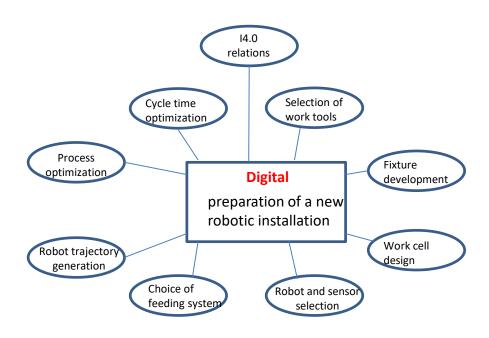
Problem: The robot systems integrator is often unable to offer even these basic digital tools

Problem: 3D CAD models of all relevant parts in the production should be available at the enduser

Problem: Unawareness of the advantages



#### Where we should be !!!





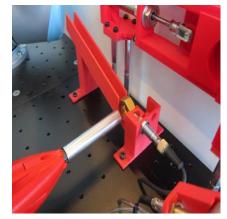
#### Three examples of digital modeling and simulation:

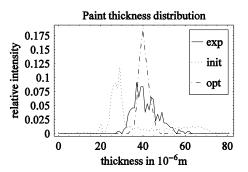














## Example 1: Bowl feeder design

#### Problem:

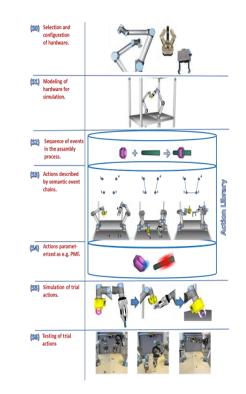
Part specific bowl feeders are implemented based on a trial and error procedure Requires very high expertise

Expensive bottleneck

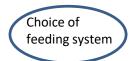
#### Solution:

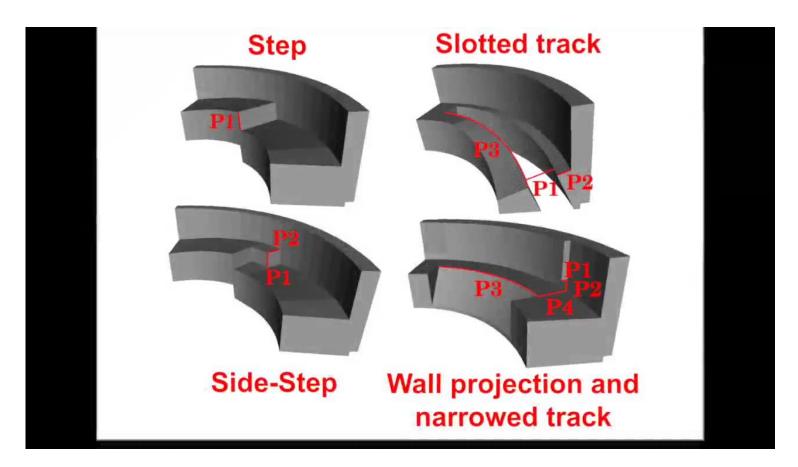
Use computer simulations as a replacement for the trial and error procedure

Reduces price and paves the way for the option of enduser designing these themselves

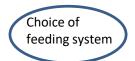








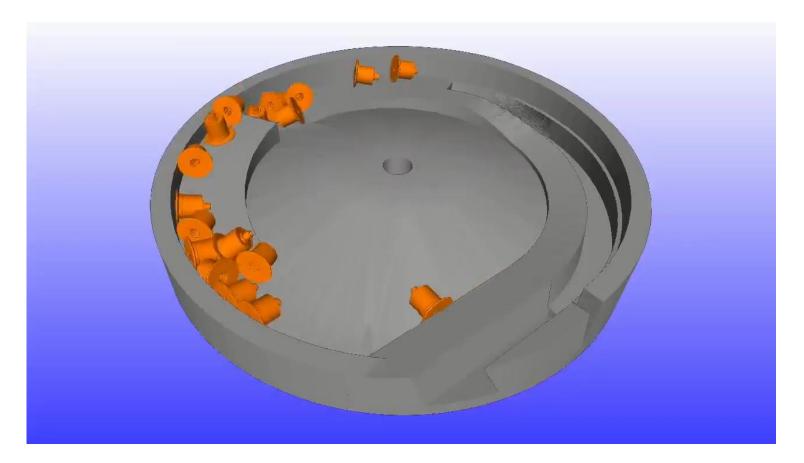




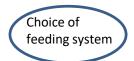


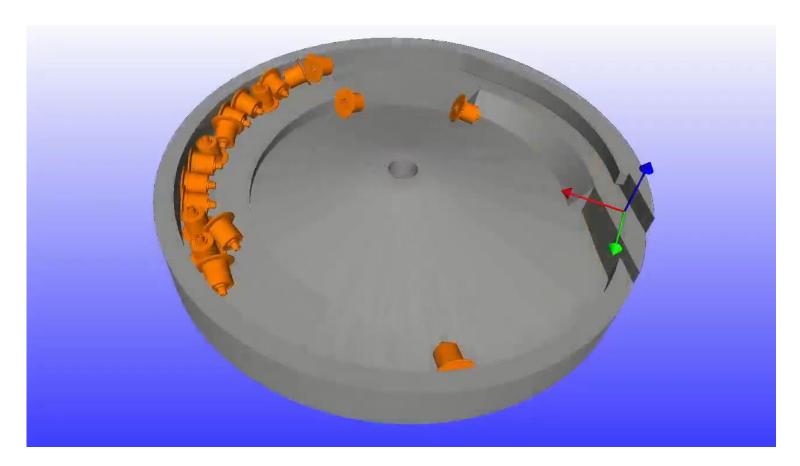




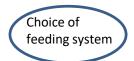
















## **Example 2: Robot Spray Painting**

#### Problem:

Double-curved surface to be painted (one of a kind)

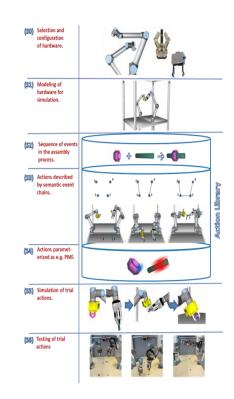
Desired thickness given

Automatical computation of spray nozzle trajectory

#### Solution:

Calibrate paint flux in spray nozzle

Compute nozzle trajectory by simulation based optimization







## Spray cone flux model

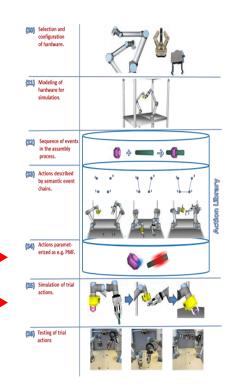
The streamlines radiate from the tool center, which ensures that the paint flux is contained within a cone whose silhouettes are straight lines,

If the cone is intersected by a plane perpendicular to the cone axis, the curves of constant flux in this plane are ellipses,

The divergence of j must be zero, which ensures that the total flux across any surface completely intersecting the cone is a constant, expressing conservation of paint.

$$\mathbf{j}(\mathbf{r}, \mathbf{u}_1 \cdots \mathbf{u}_3) = \alpha Q((\mathbf{r} \cdot \mathbf{u}_3)/(\mathbf{r}^T \mathbf{A} \mathbf{r})^{1/2})\mathbf{r}/(\mathbf{r}^T \mathbf{A} \mathbf{r})^{3/2}$$

$$\mathbf{A} = \mathbf{u}_1(t)\mathbf{u}_1(t)^T + \alpha^2\mathbf{u}_2(t)\mathbf{u}_2(t)^T + \mathbf{u}_3(t)\mathbf{u}_3(t)^T$$

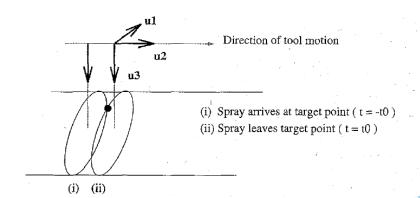




#### Finding the flux parameters of the nozzle by calibration

- Paint flat surface
- Constant distance and speed
- Spray gun perpendicular to surface

$$c(u,v)dA = -\int_{-\infty}^{\infty} \mathbf{j}(\mathbf{r}(u,v) - \mathbf{r}_{TC}(t), \mathbf{u}_{1}(t), \mathbf{u}_{2}(t), \mathbf{u}_{3}(t)) \cdot (\mathbf{r}_{u}(u,v) \times \mathbf{r}_{v}(u,v)) du dv dt$$



# After several shifts of variables and some tedious algebra...

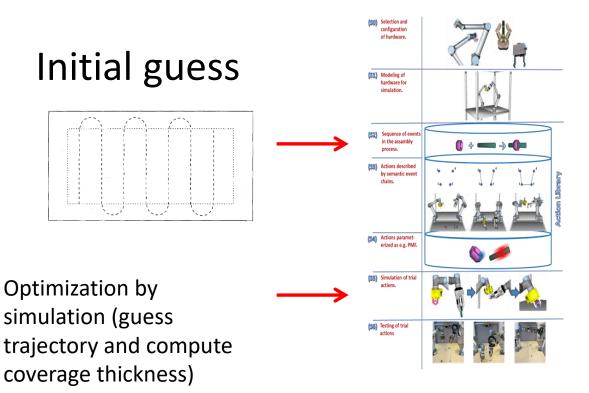
$$C(w) = \int_0^w \frac{q(u)}{\sqrt{w - u}} du.$$

Analytical solution apparently first found by N.H. Abel in 1823:

$$q(u) = \frac{1}{\pi} \int_0^u \frac{C'(\eta)d\eta}{\sqrt{u - \eta}}.$$



# Optimizing the nozzle trajectory





# Painting a wheelbarrow

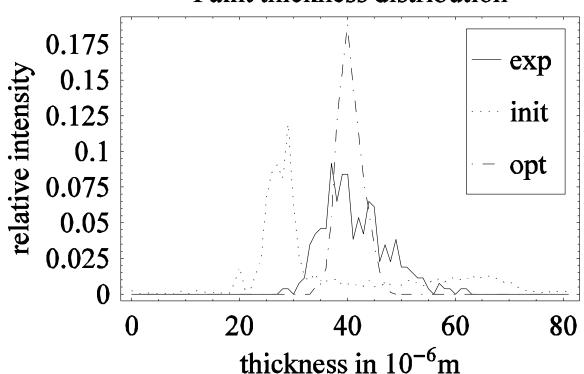






### Simulation and experimental results







# Example 3: Dynamic simulation models for robust robot assembly



# Example 3: Dynamic simulation models for robust robot assembly

#### Problem:

Optimizing assembly operations on site can be difficult because errors are rare.

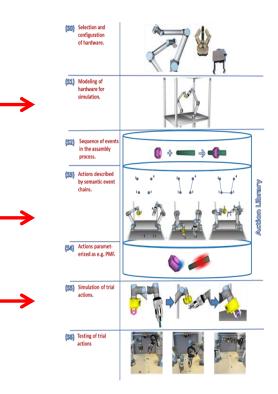
Hence the run-in time is long

Process is poorly understood

#### Solution:

Use computer simulations as a supplement for the trial and error procedure

Requires a process model and hence forces process understanding

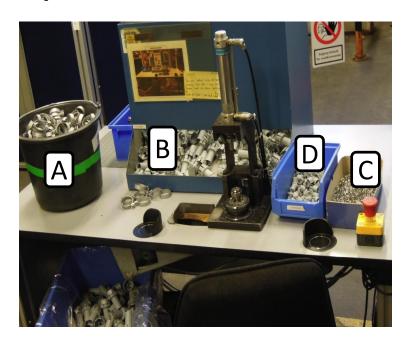




# Usage: Simple movable, reconfigurable, adaptable platforms



Movable and reconfigurable



Adaptable to randomly located parts



## An example of a simple task

- Posed by the company KVM-Conheat
- Task: Place the two union nuts on the pipe as shown
- Several steps in the task, but main here is on getting the nuts onto the pipe
- Pipe and nut feeders used

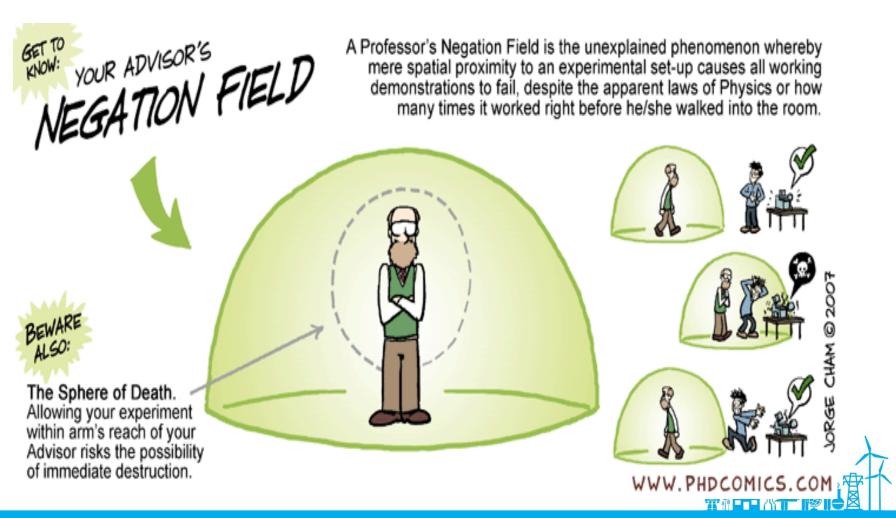




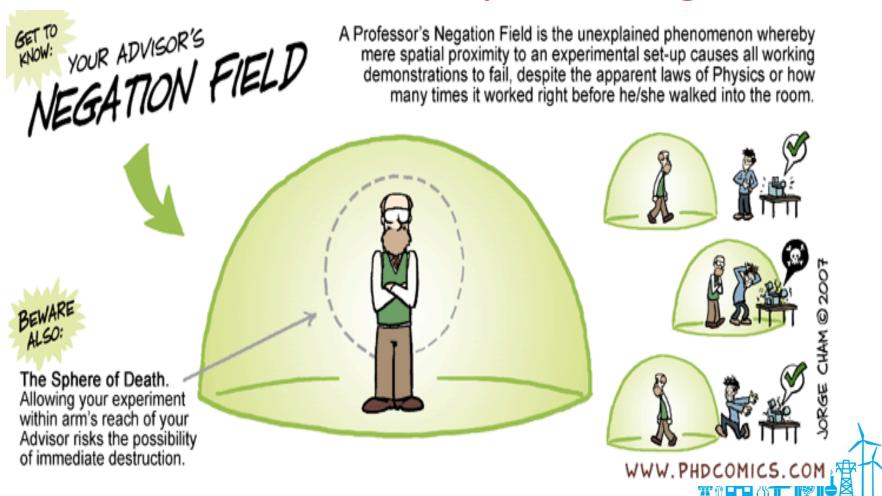
# Conventional teach-in programming of the task



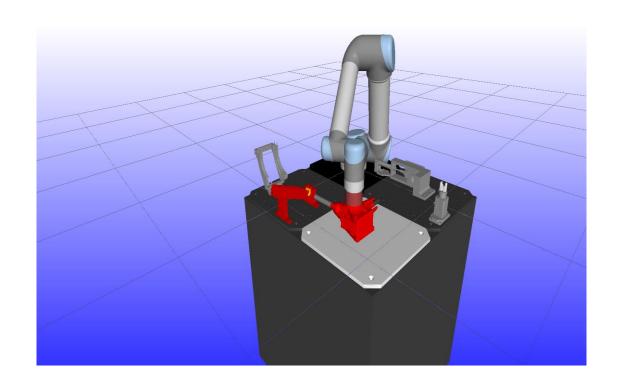
## Professor's negation field:

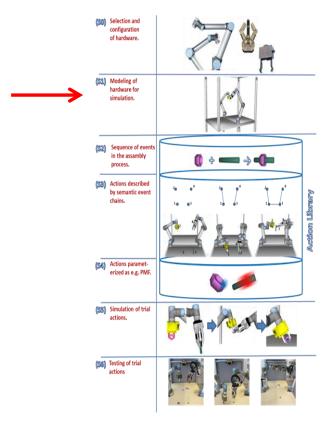


# Professor's negation field: Lack of uncertainty handling



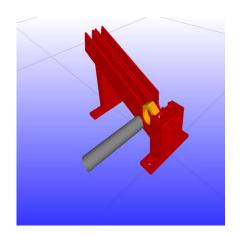
### Modeling of hardware for simulation



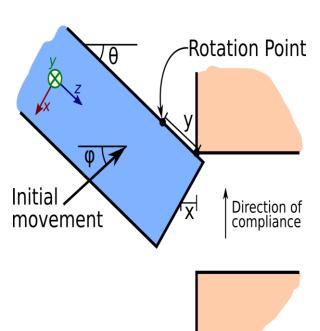


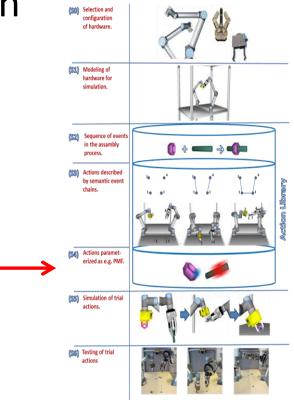


### Action parametrization







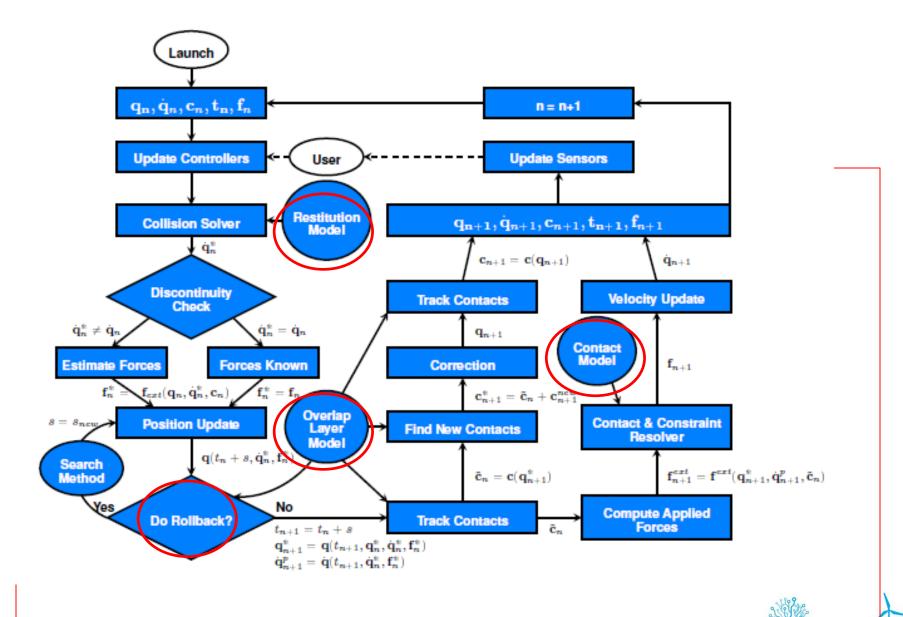




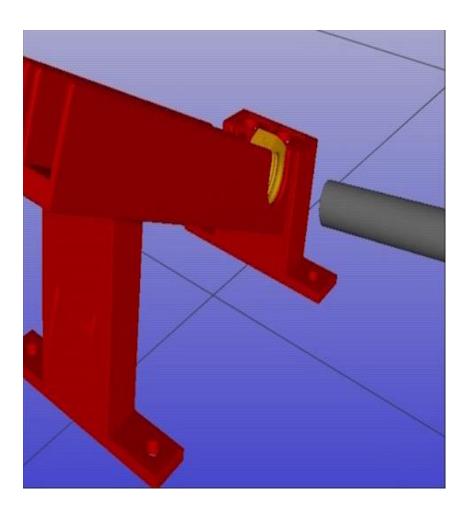
### Dynamic simulations

- Newton/Euler rigid body equations of motion
- Bodies modeled as rigid
- Contact models (friction, restitution)
- Existing engines too inaccurate (aimed for computer games)

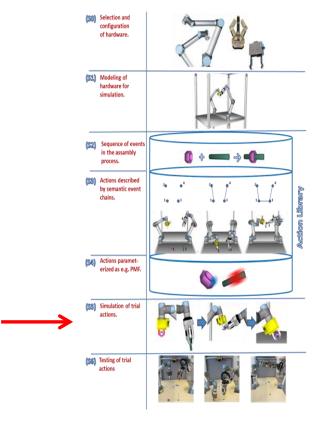




#### Simulation of trial actions:

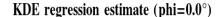


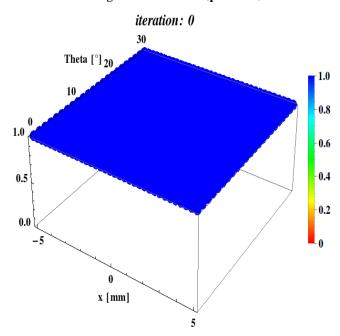
A chosen set of action parameters A randomly chosen pose perturbation





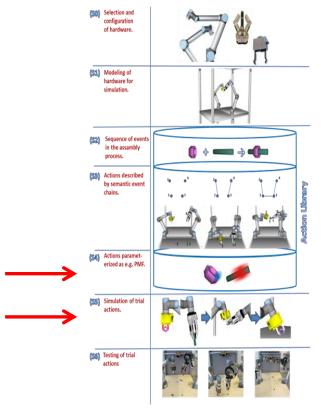
#### Learning promising action parameters:





$$\hat{\mu}_{H}(x) = \frac{\hat{p}_{O}(x,s)}{\hat{p}_{X}(x)} = \frac{n^{-1} \sum_{i=1}^{n} K_{H,x_{i}}(x) O_{i}}{n^{-1} \sum_{j=1}^{n} K_{H,x_{j}}(x)} \qquad CI_{kde} = z \cdot \sqrt{\frac{||K||_{2}^{2} \hat{\sigma}_{H}^{2}(x)}{n |H| \hat{f}_{H}(x)}}$$

$$CI_{kde} = z \cdot \sqrt{\frac{||K||_2^2 \hat{\sigma}_H^2(x)}{n |H| \hat{f}_H(x)}}$$





## Learned solution

